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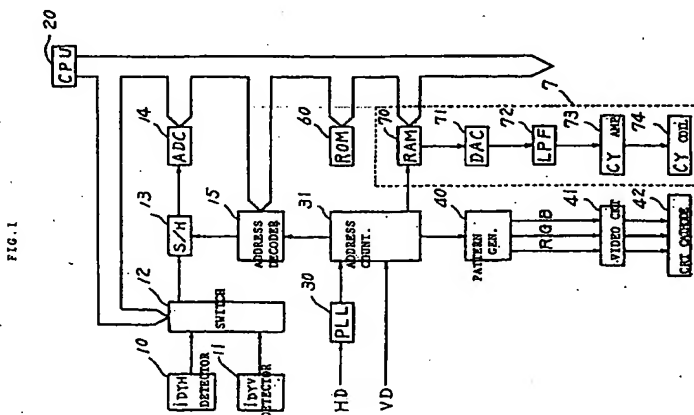
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Background of the Invention

The present invention relates to an image correction system for a cathode ray tube (CRT) display such as a color television receiver or a display terminal and, particularly, to a digital image correction device for use in a multi-mode CRT display device having a plurality of display modes which are different from each other in electron beam deflecting condition.

As an example of a conventional digital image correction device, a digital convergence correction device responsible to any of a plurality of signal specifications is disclosed in Japanese Patent Application Laid-open (Kokai (P)) No. 61-222392.

In the disclosed digital convergence correction device, convergence correction data of regulation points are stored in a memory and a read address timing is controlled by respective input signals so that a location of regulation point on an image screen is always maintained fixed. However, this prior art is silent of the difficulty of maintaining the regulation point at such fixed location by independently controlling timing of the respective regulation points. Further, in such system in which all of regulation points are controlled evenly, accuracy of correction is not enough and thus it is necessary to reregulate them every input signal or every change of raster size.

SUMMARY OF THE INVENTION

An object of the present invention is, therefore, to provide an image correction device for use in a multi-mode display device which performs an image correction including convergence correction.

Another object of the present invention is to provide a digital convergence correction device capable of accurately responding to change of display signal specification or raster size by a single regulation without necessity of re-regulation and a regulation method therefor.

In order to achieve the above objects, according to the present invention, convergence correction data or image correction data and horizontal and vertical deflection currents corresponding thereto in a mode which is used as a reference mode for respective regulation points are stored and convergence correction data or image correction data suitable for the deflection currents of the respective regulation points at that time is calculated on the basis of correlation between the deflection currents and the convergence correction data (image correction data) in the reference mode when the mode is changed, that is, when display signal specification or raster size is changed.

With the above mentioned scheme in which convergence correction data (image correction data) of regulation points are obtained by calculation, there is no troublesome address control required and, for example, timing of the regulation points may be at equidistant interval which is the simplest.

Further, since the present invention utilizes correlation between deflection currents which have a 1 : 1 correspondence to positions on an image screen and convergence correction data (image correction data), it is possible to obtain a convergence correction data for each position of the regulation points independently even if positions of the regulation points are changed, resulting in high correction accuracy. Therefore, by once regulating them in a reference mode, there is no need of re-regulation for any succeeding change of mode."

BRIEF DESCRIPTION OF THE DRAWINGS

The above-mentioned and other objects, features and advantages of the present invention will become more apparent from the following detailed description when taken in conjunction with the accompanying drawings, wherein:

Fig. 1 shows a block circuit diagram showing a construction of a first embodiment of the present invention;

Fig. 2 shows an example of display before and after convergence regulation;

Fig. 3 shows a relation between regulation points and correction points;

Fig. 4 is a flowchart of convergence regulation according to the first embodiment;

Fig. 5 shows a relation between regulation point and various modes;

Fig. 6 illustrates a linear interpolation;

Fig. 7 illustrates high order interpolation;

Fig. 8 shows a relation between deflection current and regulation point;

Fig. 9 is a first example of a deflection current detection circuit;

Fig. 10 is a second example of a deflection current detection circuit;

Fig. 11 shows a construction of a second embodiment of the present invention;

Fig. 12 shows a construction of a third embodiment of the present invention;
 Fig. 13 illustrates an image distortion at a time when raster size is changed;
 Fig. 14 shows a construction of a fourth embodiment of the present invention; and
 Fig. 15 is a schematic block diagram of a projection type display device having a digital convergence
 correction device according to the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Fig. 1 shows a construction of a first embodiment of a digital convergence correction device according to the present invention. In Fig. 1, the digital convergence correction device includes a central processing unit (CPU) 20, a first detection circuit 10 for detecting a horizontal deflection current i_{DH} flowing through a horizontal deflection coil of a CRT of a display device, a second detection circuit 11 for detecting a vertical deflection current i_{DV} flowing through a vertical deflection coil thereof, an analog data switching circuit 12 for receiving analog signals from the detector circuits 10 and 11 and outputting either one of the analog signals under control of the CPU 20, a sample-hold circuit 13 for sampling/holding the analog signal from the switching circuit 12 under control of the CPU 20 according to sampling pulses supplied thereto, an analog to digital converter (ADC) 14 for converting an output analog signal from the sample-hold circuit 13 into a digital signal under control of the CPU 20, a phase locked loop (PLL) circuit 30 for multiplying a horizontal synchronizing signal HD to generate a basic clock signal, an address counter 31 responsive to a vertical synchronizing signal VD to count the basic clocks from the PLL circuit 30 to thereby generate an address signal, an address decoder 15 for decoding the address signal from the address counter 31 and generating the sampling pulses, a pattern generator 40 responsive to the address signal from the address counter 31 for generating a display pattern for convergence regulation and a video circuit 41 connected to CRT cathode device 42.

The CPU controls an operation of the whole digital convergence correction system including peripheral input devices (keyboard, etc.), an electrically erasable and programmable read only memory (EEPROM) 60 for storing convergence correction data of regulation points in a reference mode, deflection currents and numerical values related thereto and a convergence correction unit 7 including a random access memory (RAM) 70 for storing convergence correction data of all of correction points (regulation point and correction point will be defined clearly later), a digital to analog converter (DAC) 71 for converting a digital signal into an analog signal, a low pass filter (LPF) 72 for removing high harmonic signal components, a convergence yoke (CY) coil 74 and a convergence yoke (CY) amplifier 73 for amplifying an output signal of the LPF 72 to drive the CY coil 74.

In operation, first, the horizontal synchronizing signal HD contained in a display signal or a signal synchronized therewith is supplied to the PLL circuit 30. The PLL circuit 30 generates the basic clock signal in response thereto. The basic clock signal is supplied together with the vertical synchronizing signal VD of the display signal or any signal synchronized therewith to the address counter 31. The address counter 31 generates addresses corresponding to vertical and horizontal time phases, that is, addresses corresponding to positions of the vertical synchronizing signals VD and the basic clock signal from the PLL 30 on an image screen. The addresses generated are input to the pattern generator 40, the address decoder 15 and the RAM 70 of the convergence correction unit 7, respectively. The pattern generator 40 functions to generate a display pattern (cross hatching, etc.) on the screen which is necessary to regulate convergence. The pattern generator 40 can on-off control displays of red, green and blue colors separately and an output of the generator 40 is, after amplified by the video circuit 41, supplied to the cathode 42 of the CRT and displayed thereon.

Fig. 2 shows an example of display of a regulation pattern before and after convergence regulation, in which dotted lines show the display before convergence regulation and solid lines show that after convergence regulation. It should be noted that Fig. 2 shows a display of only one of red, green and blue colors for simplicity of illustration. A cross hatching is provided as reference and convergence regulation is performed such that lattice points (regulation points) of red, green and blue colors are overlapped with lattice points of the reference cross hatching, respectively. The convergence correction data of them are written in the ROM 60.

Now, a relation between regulation point and correction point will be described with reference to Fig. 3 in which positions of respective regulation points and correction points are plotted on an image screen after convergence regulation. In Fig. 3, circles indicate regulation points and respective cross points indicate correction points. Individual correction data can be set at the respective correction points from which convergence correction data are derived. On the other hand, regulation points are set at selected ones of correction points, at which convergence regulation is actually performed. That is, regulation is performed at

regulation points each being a representative of a certain number of correction points and, for other correction points, their correction data are obtained by interpolation on the basis of correction data of the regulation points. In the shown example, interpolation is performed by software by means of the CPU 20. In this case, correction accuracy is degraded when distance between adjacent regulation points is large.

5 Therefore, in order to avoid such degradation of correction accuracy, it is desirable to increase the number of regulation points. However, the number of regulation points should be as small as possible in view of time required to perform interpolation. Although time, image screen position or deflection currents, etc., may be usable as variables of the interpolation function, it is usual to use time as variable in view of convenience of variable management. In view of possibility of optimizing time constant of the LPF 72, possibility of
10 simplifying interpolation and easiness of managing time as variable, inter-correction point distance and inter-regulation point distance are made equal in time, respectively.

Convergence correction data of respective correction points thus obtained are written in predetermined addresses of the RAM 70 shown in Fig. 1 corresponding to positions on an image plane and then read out by output addresses of the address counter 31 correspondingly to the image plane positions within one
15 vertical scan period. The digital convergence correction data thus read out are converted by the DAC 71 into analog signals. The analog signal whose high harmonic components are removed by the LPF 72 is converted by the CY amplifier 73 into a predetermined current to be flown through the CY coil 74.

The convergence correction units 7 correspond in number to convergence correction systems, that is, the CY coils 74. For example, in a case of a projection type television receiver, horizontal and vertical
20 convergence regulation functions are required for each of at least green and blue colors, that is, at least four convergence correction units 4 are required. Further, convergence regulation function for red color is necessary to make correction of graphic distortion possible with this system. In such case, the number of required convergence correction units becomes six.

A sufficient convergence correction is possible by this method for a certain display mode. However,
25 since positions of regulation points on an image plane may be changed in another mode in which raster size and/or signal specification is different from those in the certain mode, it is not always possible to correct convergence in such mode. Therefore, in such case, it is not always possible to use convergence correction data written in the ROM 60 as they are.

In order to solve this problem, in the present invention, deflection currents having a 1 : 1 correlation to
30 each position on the image plane are stored together with the convergence correction data concerning to that position, in the ROM 60. Thus, even if a position of the regulation points is changed, convergence correction data suitable for that position can be obtained by reading the deflection currents at that position in the ROM 60 and performing an interpolation using the correlation between deflection currents and the convergence correction data.

35 The horizontal deflection current detection circuit 10 and the vertical deflection current detection circuit 11 pick up horizontal and vertical deflection currents i_{DH} and i_{DV} flowing through the DY coils as voltages, respectively. One of the voltages is selected by the switching circuit 12 and supplied to the S/H circuit 13.

The address decoder 15 decodes an output address of the address counter 31 and outputs sampling pulses to the sample/hold circuit 13 at timing of a single regulation point determined by the CPU 20. The
40 sample/hold circuit 13 samples a deflection current value (converted into voltage value) at the regulation point determined by the CPU 20 and the sampled analog value is converted into a digital value by the ADC 14 and read in the CPU.

The above mentioned regulation method of convergence using the present system is summarised in a flowchart shown in Fig. 4. In a convergence correction system of a display device having a plurality of
45 display modes different in raster size and signal specification from each other, Mode 1 is first selected as a reference mode (step S1) on which a convergence regulation is performed to set convergence correction data of a regulation point (step S2) and then convergence correction data at respective correction points are obtained by time interpolation and written in the RAM 70 (step S3). In the step S4, regulation is repeated if an error of convergence is larger than an acceptable amount. Otherwise, the regulation is terminated and
50 deflection currents at respective regulation points are read (step S5) and written in the ROM 60 together with convergence correction data (step S6).

When a mode other than the reference mode is to be displayed, a mode switching is performed (step S7) and deflection currents at respective regulation points in that mode are read in (step S8) on which convergence correction data of the respective regulation points are obtained by interpolation utilizing the
55 correlation between convergence correction data of the regulation points in Mode 1 and deflection currents (step S9). On the basis of thus obtained convergence correction data of the regulation points, convergence correction data of respective correction points are obtained by time interpolation in the same manner as in Mode 1 (step S10) and written in the RAM 70 (step S11). In this example, the above mentioned operations

(steps S7 to S11) are performed every mode change (step S12).

Although this system requires a certain time for interpolation at every mode switching, the memory cost can be restricted. On the other hand, there is another method in which enough memory regions of the RAM 70 are kept for respective modes and convergence correction data at respective correction points are preliminarily calculated and written in the memory regions, respectively. In such case, although memory size may be increased, it is possible to match convergence immediately at mode switching. In addition, if convergence correction data of regulation points for respective modes are stored in the ROM, it is possible to reduce time necessary for interpolation.

As mentioned, according to this embodiment, once convergence regulation for one mode as the reference is performed, it is possible to obtain convergence correction data suitable for that mode by interpolation based on the correlation between the convergence correction data of the reference mode and deflection currents by merely reading in deflection currents of respective regulation points in any other mode. Thus, a maximum correction accuracy can be obtained. Therefore, procedure required for convergence regulation can be substantially reduced. This effect is advantageous when the number of display modes increases. Further, since this embodiment utilizes a combination of interpolation using deflection current as parameter and interpolation using time as parameter, both a high correction accuracy and a reduction of operation time are achieved simultaneously.

Now, how to obtain convergence correction data of regulation points in other mode than the reference mode, that is, how to perform interpolation therefor, will be described in detail with reference to Fig. 5 which shows cross-hatch images of two modes, Mode 1 and Mode 2, which are different in raster size. Regulation points in Mode 1 which is a reference mode are represented by P and those in mode 2 are depicted by P'. The number of regulation points is n(horizontal) X m(vertical), where n and m are positive integers. It is known that reliability of data obtained by extrapolation is generally lower than that of interpolation. Therefore, raster size of the reference Mode 1 should be enough to make interpolation possible.

There are two methods for obtaining correction data of a regulation point P'(k, l) in Mode 2. In the first one of these methods, one of square-like areas of the cross hatch having lattice points as the regulation points P in Mode 1 including a regulation point P'(k, l), is determined and then correction data of the point P'(k, l) is obtained by locally performing interpolation in and around that square-like area on the basis of deflection currents. In a second method, the correction data is calculated on the basis of the correlation between convergence correction data of all of the regulation points in Mode 1 and deflection currents.

In detail, in the first method, that square-like area of the cross hatch in Mode 1 which includes the regulation point P'(k, l) in Mode 2 is determined by sequentially comparing horizontal deflection current and vertical deflection current at the regulation point P'(k, l) with those at respective regulation points in Mode 1 and the convergence correction data of the regulation point P'(k, l) is obtained by performing interpolation in and around that square-like area on the basis of deflection currents. Since, in this method, such area is preliminarily determined, such local interpolation does not produce any problem.

Fig. 6 illustrates an example of interpolation (linear interpolation) in that square-like area. Assuming that P'(k, l) in Mode 2 exists in an area having apices defined by regulation points P(i, j), P(i+1, j), P(i, j+1) and P(i+1, j+1) in Mode 1, a vertical deflection current i_{VT} of a point T which has the same horizontal deflection current value as that of the point P'(k, l) and a convergence correction data CD_T are obtained by linear interpolation from the relations between vertical deflection currents $i_V(i, j)$ and $i_V(i+1, j)$, horizontal deflection currents $i_H(i, j)$ and $i_H(i+1, j)$ and convergence correction data $CD(i, j)$ and $CD(i+1, j)$ of points P(i, j) and P(i+1, j) according to the following equations:

$$i_{VT} = \{(i_H(i+1, j) - i_H(k, l))i_V(i, j) + (i_H(k, l) - i_H(i, j))i_V(i+1, j)\} / \{i_H(i+1, j) - i_H(i, j)\} \quad (1)$$

$$CD_T = \{(i_H(i+1, j) - i_H(k, l))CD(i, j) + (i_H(k, l) - i_H(i, j))CD(i+1, j)\} / \{i_H(i+1, j) - i_H(i, j)\} \quad (2)$$

Similarly, a vertical deflection current i_{VB} of a point B which has the same horizontal deflection current value as that of the point P'(k, l) and a convergence correction data CD_B are obtained by linear interpolation from the relations between horizontal deflection currents $i_H(i, j+1)$ and $i_H(i+1, j+1)$, vertical deflection currents $i_V(i, j+1)$ and $i_V(i+1, j+1)$ and convergence correction data $CD(i, j+1)$ and $CD(i+1, j+1)$ of points P(i, j+1) and P(i+1, j+1) according to the following equations:

$$i_{VB} = \{(i_H(i+1, j+1) - i_H(k, l))i_V(i, j+1) + (i_H(k, l) - i_H(i, j+1))i_V(i+1, j+1)\} / \{i_H(i+1, j+1) - i_H(i, j+1)\} \quad (3)$$

$$CD_B = \{(i_H(i+1, j+1) - i_H(k, l))CD(i, j+1) + (i_H(k, l) - i_H(i, j+1))CD(i+1, j+1)\} / \{i_H(i+1, j+1) - i_H(i, j+1)\} \quad (4)$$

Thereafter, convergence correction data $CD'(k,l)$ for vertical deflection current value $i_v(k,l)$ of point $P'(k,l)$ is obtained by linear interpolation from relations between convergence correction data CD_T and CD_B and respective vertical deflection currents i_{vT} and i_{vB} of the points T and B according to the following equation:

$$CD'(k,l) = \{(i_{vT} - i_v(k,l))CD_B + (i_v(k,l) - i_{vB})CD_T\} / \{i_{vT} - i_{vB}\} \quad (5)$$

According to this embodiment which utilizes both the deflection current comparison and linear interpolation, a high speed arithmetic operation is possible. However, in order to keep correction accuracy high, it is necessary to increase the number of regulation points to some extent. Alternatively, it is necessary to increase order of interpolation function by expanding the area to be interpolated and, after a square-like area is obtained, performing interpolation of the area including regulation points around the area.

Although, in the example shown in Fig. 6, the interpolation using horizontal deflection current is performed first to obtain data of the points T and B and then interpolation of vertical deflection current is performed, it is possible to perform interpolation of vertical deflection current first to obtain data of points L and R and then perform interpolation using horizontal deflection current.

The second method will be described with reference to Fig. 7 which illustrates a second example of interpolation of deflection current. Unlike the first method, the second method utilizes correlation between correction data and deflection currents of regulation points on a whole image plane to obtain convergence correction data of a new regulation point. The second method may be considered as one in which a square-like area in the first method is expanded up to the whole image plane to increase the order of interpolation. Since the square-like area is the whole image plane, there is no need of area selection and it is enough to perform interpolation. First, convergence correction data $D_v(j)$ and vertical deflection current $i_v(j)$ of a point $TB(j)$ having the same horizontal deflection current $i_H(k,l)$ as that of regulation point $P'(k,l)$ in a currently employed mode are obtained from correlation between horizontal deflection currents $i_H(0,j) - i_H(n-1,j)$ and convergence correction data $CD(0,j) - CD(n-1,j)$ of regulation points $P(0,i) - P(n-1,j)$ in line j in the reference mode. This is performed for every regulation point in the reference mode and convergence correction data $D_v(0) - D_v(m-1)$ and vertical deflection currents $i_v(0) - i_v(m-1)$ of points $TB(0) - TB(m-1)$ having the same horizontal deflection current as $i_H(k,l)$ of a certain regulation point $P'(k,l)$ in the current mode are obtained by interpolations. Then, convergence correction data $CD'(k,l)$ for the same vertical deflection current $i_v(k,l)$ as that of the certain regulation point $P'(k,l)$ is obtained by interpolation from correlation between convergence correction data $D_v(0) - D_v(m-1)$ and vertical deflection currents $i_v(0) - i_v(m-1)$ thus obtained for one line. Since this utilizes a high order interpolation on the basis of information of the whole image plane, it is possible to interpolate smoothly even if the number of regulation points is relatively small. In this case, interpolations using vertical deflection current first and then horizontal deflection current as parameters can be performed in the order. Further, in both the first and second methods, when a variation of vertical deflection current within one scan line is small, vertical deflection currents of regulation points in each line can be represented by a vertical deflection current at any one point in the line, so that it is possible to reduce read-in time of deflection current, operation time and ROM capacity, etc.

Although the regulation point has been described as the same as deflection current read-in point, it is not always necessary to set them at the same point. It is possible to select any suitable point among correction points, read deflection data thereinto and perform interpolation using correlation between the deflection current read-in and convergence correction data at that point.

In general, when the number of regulation points is n, the order of interpolation function becomes n-1. A correlation equation between deflection current and convergence correction data can be obtained by inserting deflection currents i and convergence correction data CD of respective regulation points into (n-1)-th order function such as shown by the following equation (6), sequentially, and by obtaining a coefficient a(j) by solving simultaneous equations thus obtained.

$$CD = \sum_{j=0}^{n-1} a(j) i^j \quad \dots\dots\dots (6)$$

Instead of solving such simultaneous equations, convergence correction data can be obtained directly by using Lagrange's interpolation formula, with the same effect.

Now, deflection current to be stored in the ROM 60 and used as a basis of the interpolation will be described with reference to Fig. 8 which shows a relation between deflection current and regulation points. This figure includes blanking periods and an area surrounded by dotted line is a portion actually displayed

on an image plane. Regulation points outside the dotted line are not regulated actually and convergence correction data thereof have to be produced by extrapolation. On the other hand, deflection currents exhibit monotonous variations within a display period. However, their variations in blanking periods are drastic. Therefore, it is impossible to obtain a correlation between convergence correction data and deflection currents in such drastically changing areas. In order to solve this problem, there is a system provided according to the present invention, in which data for deflection currents in the blanking period is produced by extrapolation and stored in the ROM 60. It is, of course, possible to store convergence correction data and deflection current for only regulation points within a display period in the ROM 60, obtain convergence correction data for the regulation points within the display period in other mode than the reference mode by using the correlation therebetween and finally obtain convergence correction data for regulation points outside the image plane by extrapolation.

The deflection current detection circuits 10 and 11 (Fig. 1) function to convert deflection currents into voltages and it is desired that they do not affect the deflection circuits substantially. Fig. 9 shows an example of construction of either deflection current detection circuit. The deflection current detection circuit comprises a current transformer whose primary winding is connected in series with the DY coil and secondary winding is connected in parallel to a resistor for conversion into voltage. Fig. 10 is another example of the deflection current detection circuit in which a resistor is connected in series with the DY coil to directly convert current into voltage. Although either of the deflection current detection circuits shown in Figs. 9 and 10 is preferable, deflection current may be detected by using a current probe utilizing a Hall element, etc. Since such current probe is usually detachable, it is possible to attach it to the device for only convergence regulation of a multi-mode display device. Such probe is not always necessary to be assembled in the device so long as convergence correction data for respective modes is preliminarily obtained by performing interpolation using deflection currents and stored in the memory. Thus, it is possible to reduce the size of deflection current detection circuitry. In this case, it should be noted that the data can not be used when operation mode stored after regulation is switched to a different mode.

Parameter which requires correction data which has a dependency on image screen position is not limited to convergence. By dynamically correcting variation of luminance, white balance and focus according to locations on the image plane, remarkable improvements on these parameters are possible.

Fig. 11 shows a construction of a second embodiment of the present invention. This embodiment is basically similar in structure to that shown in Fig. 1 and same reference numerals in Fig. 11 depict same constitutional components as those shown in Fig. 1, respectively. This embodiment differs from the embodiment in Fig. 1 in that it includes, in addition to a convergence correction unit 7, a video correction unit 8 and a focus correction unit 9. Therefore, only those units 8 and 9 will be described.

The focus correction unit 9 has a similar construction to the convergence correction unit 7 except that a focus coil and a focus coil drive amplifier are used instead of the CY coil 74 and the CY amplifier 73 of the convergence correction unit 7, respectively.

The video correction unit 8 has also a similar construction to that of the convergence correction unit 7 except that the CY amplifier 73 and the CY coil 74 of the unit 7 are removed so that an output of the LPF 72 is directly supplied to an input of a control terminal of the video circuit 41.

Regulation method and operation of the digital circuit portion of each of the video correction unit 8 and the focus correction unit 9 are similar to those for the convergence correction unit 7 and only differ from the unit 7 in object to be corrected and a circuit constructions next to analog conversion.

The correction object of the video correction unit 8 is luminance of respective red, green and blue colors and contrast and the correction object of the focus correction unit 9 is focus, that is, current flowing through focus coil. According to this embodiment, in addition to the convergence correction, luminance variation, white balance variation and focus variation can be regulated favorably regardless of signal specification and raster size and it is enough to perform a regulation for only one mode.

As shown in Fig. 2, the raster shape is subjected to a pin type distortion under no correction, the larger the distortion resulting in the larger amount of convergence correction and hence the larger power consumption.

Therefore, it is conventional to reduce pin type distortion by amplitude-modulation of deflection currents.

In such case where pin type distortion is reduced by amplitude-modulating, for example, horizontal deflection current, if only vertical deflection size is varied, a barrel type distortion is produced as shown in Fig. 13. That is, the barrel type distortion is due to the fact that an amount of modulation before vertical deflection size is varied is kept as it is even after the variation.

In a usual interpolation utilizing correlation between convergence correction data and deflection current, this distortion of image can not be corrected although convergence can be corrected.

Fig. 12 shows a construction of a third embodiment of the present invention which is suitable to solve this problem. In this embodiment, in addition to a convergence correction unit 7, a deflection circuit 5 and a power sensor 6 are connected to a CPU 70.

In the embodiment shown in Fig. 12, the deflection circuit 5 is controlled according to deflection size. Since deflection current can be read in a memory according to this system, an amount of modulation of the deflection circuit is controlled according to the deflection size read out from the memory. Further, since deflection size as well as position of deflection center is also closely related to convergence correction amount, they should be optimized according to a display condition. To this end, the power sensor 6 is provided to control deflection amplitude and center position of deflection such that power consumption becomes minimum.

According to this embodiment, correction of image distortion and reduction of power consumption are possible in addition to the convergence correction similar to that obtainable in the embodiment shown in Fig. 1.

Fig. 14 shows a fourth embodiment of the present invention. This embodiment differs from the first embodiment shown in Fig. 1 in two points, these points will be described below:

(1) An interpolation circuit 4 is provided separately from the CPU which is dedicated to interpolation for obtaining regulation point data in other mode than the reference mode by utilizing correlation between deflection current and convergence correction data and interpolation for obtaining convergence correction data of respective correction points from convergence correction data of regulation points. It is general that the higher the accuracy of interpolation requires the longer time. This interpolation circuit 4 is effective in reducing operation time while keeping the accuracy.

(2) Sampling pulses from an address decoder 15 for sampling deflection current is input to a pattern generator circuit 40 to mix them to a display pattern signal so that they can be displayed on a same image screen.

In order to maintain correction accuracy, matching of sampling timing of deflection current with timing for controlling timing of raster correction with convergence correction data is very important in this system. Particularly, since deflection current drastically changed in blanking periods, mismatching between these timing may cause correlation between deflection current and convergence correction data to be broken. By allowing the sampling pulses to be confirmed on the image screen, correlation between deflection current and convergence correction data can be maintained, making highly accurate correction possible.

Fig. 15 shows an example of a display device which is of a projection type display device and includes the digital convergence correction device according to the present invention. In Fig. 15, the display device comprises a convergence correction device 100 which may be constructed according to the first embodiment shown in Fig. 1, a remote controller 200 for convergence regulation, a horizontal and vertical deflection circuit 300, three CRTs 600 for producing basic three colors, red, green and blue, respectively, a mirror 500 and a screen 400 for projecting an image. Three color images from the CRTs 600 are projected through the mirror 500 onto the image screen 400 while enabling correction of image distortion by means of a convergence yoke (CY) provided for each CRT. Therefore, a total of 6 convergence correction units each such as shown by the dotted line in Fig. 1 are required to perform corrections in horizontal and vertical directions for the CRT's.

Convergence regulation is performed by the remote controller 200 operated by an operator while looking at the image screen.

As described hereinbefore, according to the present invention in which convergence correction data (image correction data) of regulation point is obtained by interpolation on the basis of deflection currents having a 1 : 1 correspondence to an image screen position, it is possible to correct convergence sufficiently even for different display modes in which raster size and/or signal specification is different. Further, since it is enough to regulate image correction for only one display mode which is reference, regulation itself can be simplified.

Although the present invention has been described with reference to the specific embodiments, this description is not meant to be construed in a limiting sense. Various modifications of the described embodiments, as well as other embodiments of the present invention, will become apparent to persons skilled in the art upon reference to the description of the present invention. It is, therefore, contemplated that the appended claims will cover any modifications or embodiments as fall within the true scope of the present invention.

Claims

1. An image correction device for use in an image display device including a display mode selector for selecting one of a plurality of different display modes and operable in any of the different display modes, comprising:
 - address generating means for generating address corresponding to positions on an image screen of said display device in synchronism with an input video signal;
 - regulation pattern generating means for generating, in synchronism with said input video signal, a regulation pattern for regulating positions of regulation points selected from correction points on said image screen;
 - first storing means for storing correction data of the correction points in address generated by said address generating means;
 - digital to analog converter means for converting a digital signal read out from said first storing means into an analog signal;
 - responsive means responsive to the analog signal for regulating parameters of a display tube of said display device;
 - deflection current detecting means for detecting deflection current flowing through deflection coils of said display device;
 - second storing means for storing the correction data and deflection currents detected by said deflection current detecting means in a reference display mode;
 - correction data generating means for generating the correction data of the correction points in a certain display mode other than the reference display mode by interpolation based on the content of said second storing means and deflection currents re-detected in the certain display mode by said deflection current detecting means and supplying the generated correction data to said first storing means; and
 - central processing means for controlling an operation of said image correction device.
2. The digital image correction device claimed in claim 1, wherein said responsive means comprises a convergence yoke driver and a convergence yoke coils and said parameter to be regulated thereby are convergence and distortion of image.
3. The digital image correction device claimed in claim 1, wherein said responsive means comprises means for supplying said analog signal from said digital to analog conversion means to a control terminal of said video circuit and said parameter to be regulated are white balance and luminance.
4. The digital image correction device claimed in claim 1, wherein said responsive means comprises a focus coil driver and a focus coil and said parameter to be corrected is focus.
5. The digital image correction device claimed in claim 1, further comprising means for detecting power dissipation of a display device, means for controlling deflection size and deflection position of said display device and means for controlling said deflection size and deflection position such that said power dissipation becomes minimum.
6. The image correction device claimed in claim 1, further comprising means for controlling image distortion correcting means of deflection circuit provided in a display device according to said deflection size read in by said deflection current detecting means.
7. An image correction device for use in an image display device, comprising:
 - address generating means for generating address corresponding to positions on an image screen of said display device in synchronism with an input video signal;
 - regulation pattern generating means for generating, in synchronism with said input video signal, a regulation pattern for regulating positions of regulation points selected from correction points on said image screen;
 - first storing means for storing correction data of the correction points in address generated by said address generating means;
 - digital to analog converter means for converting a digital signal read out from said first storing means into an analog signal;
 - responsive means responsive to the analog signal for regulating parameters of a display tube of

said display device;

deflection current detecting means for detecting deflection current flowing through deflection coils of said display device;

second storing means for storing the correction data and deflection currents detected by said deflection current detecting means in a reference display mode;

correction data generating means for generating the correction data of the correction points by interpolation utilizing correlation between said deflection currents and image correction data corresponding to said deflection currents when deflection currents of correction points are changed due to change of a scan condition of the display device and supplying the generated correction data to said first storing means; and

central processing means for controlling an operation of said image correction device.

8. The image correction device claimed in claim 1, wherein said first storing means stores image correction data and deflection currents for a plurality of points on the image screen in a display mode in which raster size is sufficiently large.

9. The image correction device claimed in claim 7, further comprising means for obtaining image correction data for a portion of respective correction points by interpolation utilizing said deflection currents as a variable and utilizing correlation between said deflection currents and image correction data corresponding to said deflection currents and obtaining image correction data for other correction points by interpolation utilizing time as a variable from said image correction data of said portion of said correction points when deflection currents of correction points are changed due to change of a scan condition of a display device.

10. The image correction device claimed in claim 1, further comprising means for detecting deflection currents in only a display period and obtaining deflection current in blanking periods by extrapolation.

11. The image correction device claimed in claim 1, wherein a linear function is used as an interpolation function.

12. The image correction device claimed in claim 1, wherein Lagrange's function is used as interpolation function.

13. The image correction device claimed in claim 1, further comprising means for displaying detection timing of deflection current on a image screen.

14. The image correction device claimed in claim 1, wherein said deflection current detecting means includes a current transformer.

15. The image correction device claimed in claim 1, wherein said deflection current detecting means detects voltage drop generated across a resistor inserted in series with said deflection coil in a display device.

16. The image correction device claimed in claim 1, wherein said deflection current detecting means includes a current probe.

17. An image display device comprising said image correction device claimed in claim 1.

18. A method of correcting convergence of a display device having a plurality of display modes different in raster size and signal specification from each other, said method comprising the steps of:

a) selecting a reference display mode;

b) regulating convergence in the reference mode to obtain convergence correction data of each of regulation points selected from a plurality of correction points on an image screen of said display device;

c) obtaining convergence correction data of each of said correction points by interpolation utilizing time as a variable on the basis of convergence correction data of the regulation points;

d) detecting deflection currents corresponding to said regulation points;

e) storing the convergence correction data of correction points in first storing means;

f) storing deflection currents at respective regulation points in said first storing means;
g) switching the corrected display mode from reference mode to a second display mode;
h) detecting deflection currents at respective regulation points in the second display mode;
i) obtaining convergence correction data of the respective regulation points by interpolation utilizing
the correlation between convergence correction data of the regulation points and deflection currents
in the reference mode;
j) on the basis of thus obtained convergence correction data of the regulation points, obtaining
convergence correction data of respective correction points by time interpolation in the same
manner as in the reference mode and storing the convergence correction data in second storing
means; and
k) correcting an image on said image screen on the basis of the content of said random access
memory.

19. The method claimed in claim 18, further comprising, between the steps c) and d), the step of:

l) checking whether the convergence correction data obtained in the step c) is satisfactory and if not
repeating the steps b) and c).

20. The method claimed in claim 19, further comprising, the step of:

m) checking whether there is a further display mode to be switched and if yes repeating the steps g)
to k).

FIG. 1

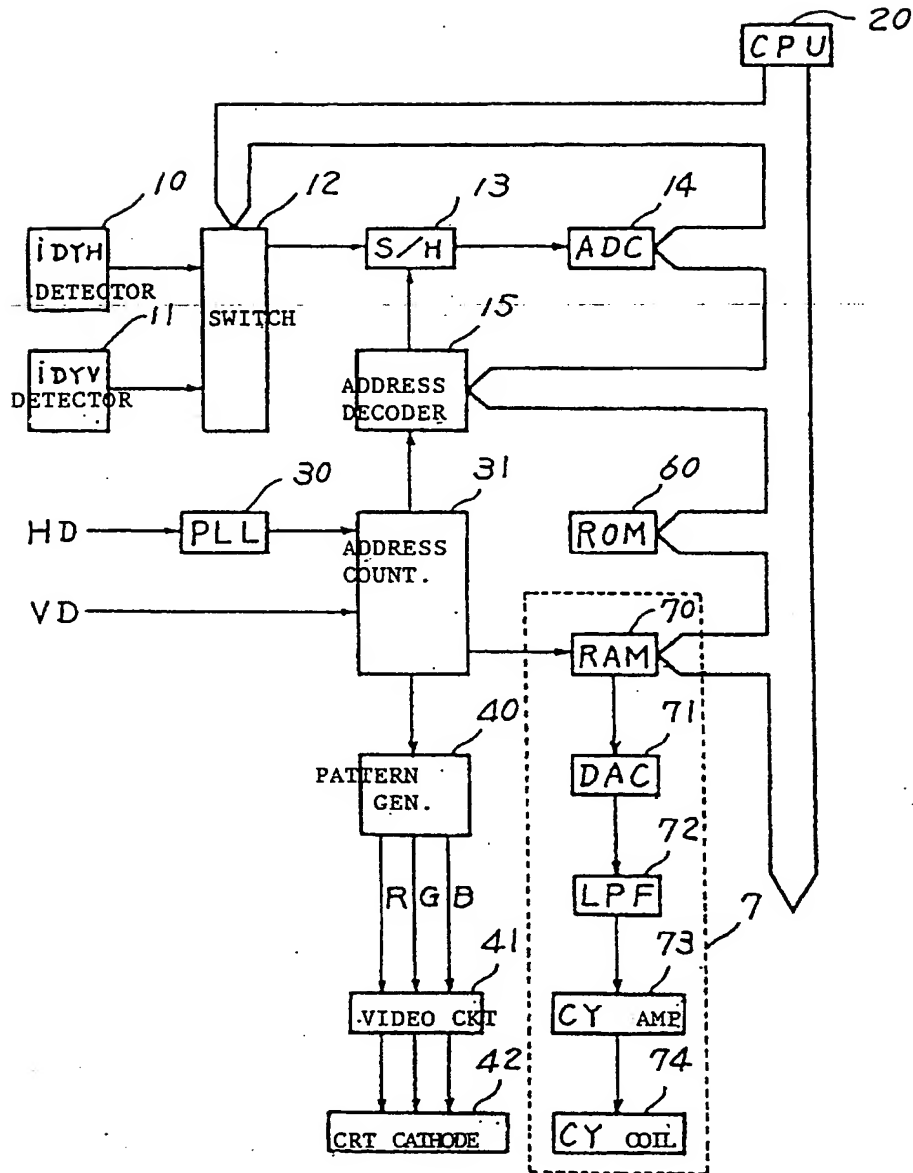


FIG. 2

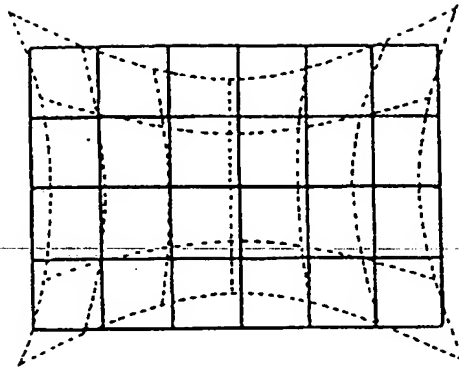


FIG. 3

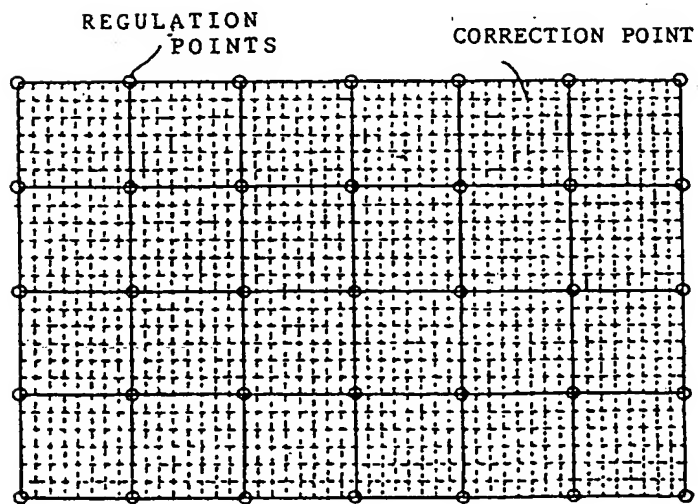


FIG. 4

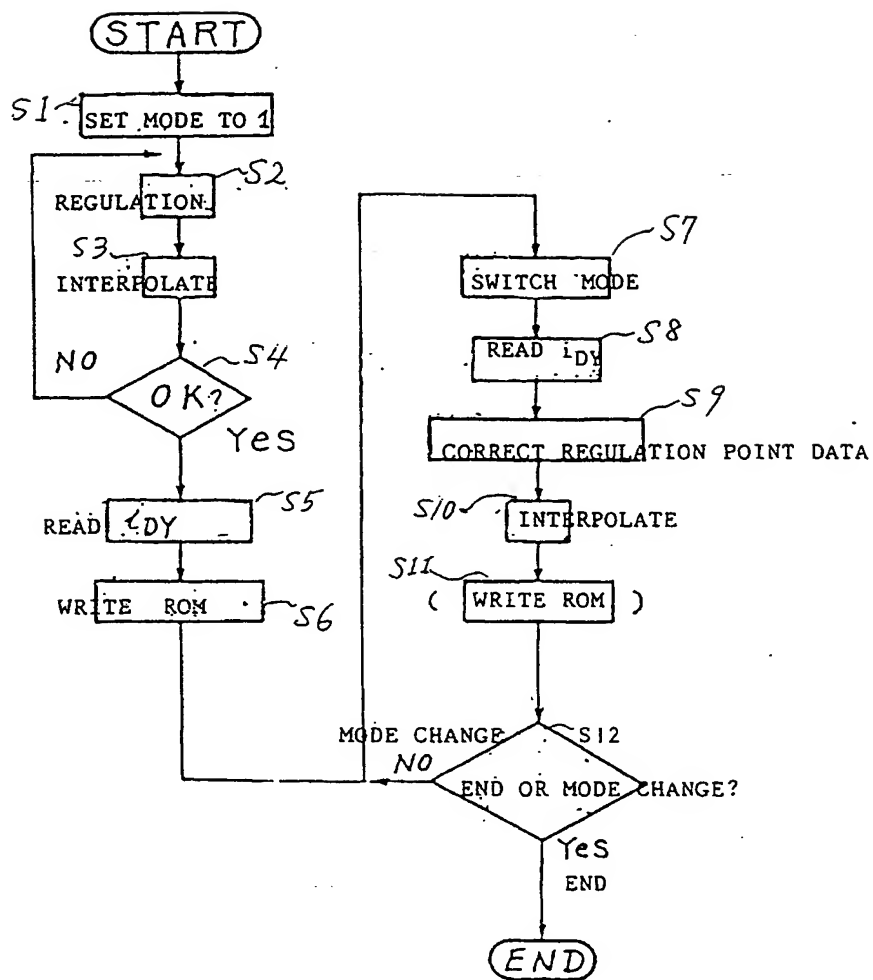


FIG. 5

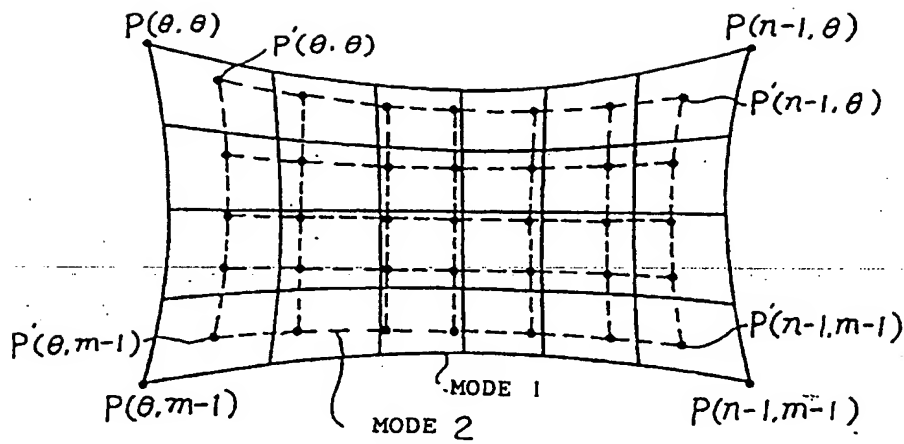
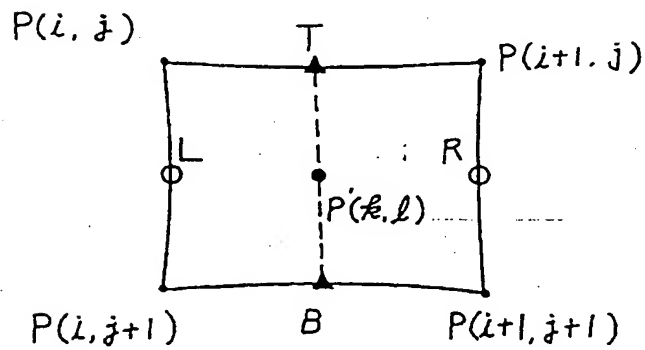


FIG. 6



A diagram illustrating a grid on a curved surface. The grid is bounded by a top curve and a bottom curve. The top-left corner is labeled $P(0, 0)$, the top-right corner is labeled $P(n-1, 0)$, the bottom-left corner is labeled $P(0, m-1)$, and the bottom-right corner is labeled $P(n-1, m-1)$. The top edge is labeled $TB(0)$ and the bottom edge is labeled $TB(m-1)$. A vertical dashed line with triangles at its intersections is labeled $P'(k, l)$ on the left. A horizontal line with circles at its intersections is labeled $P(0, j)$ on the left and $P(n-1, j)$ on the right. A point on the vertical dashed line is labeled $P'(k, l)$.

FIG. 8

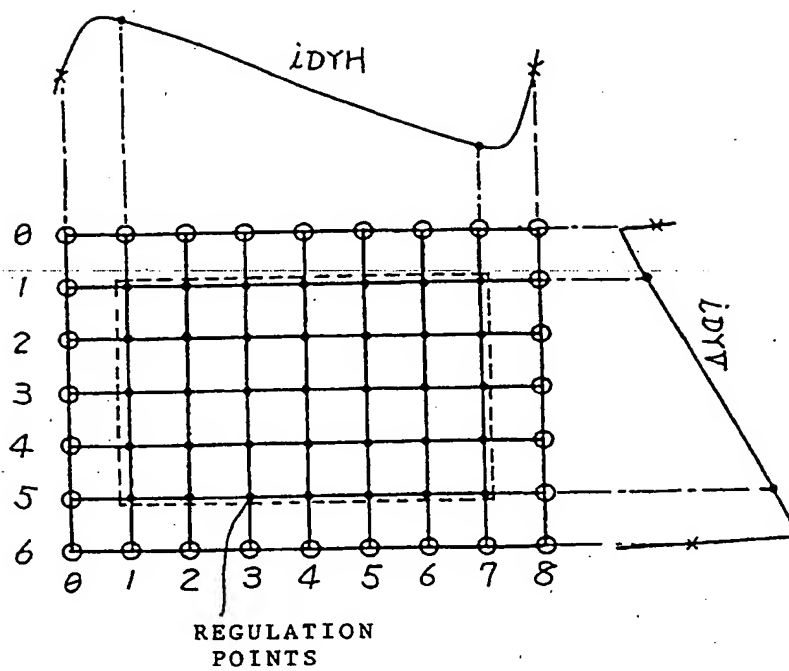


FIG. 9

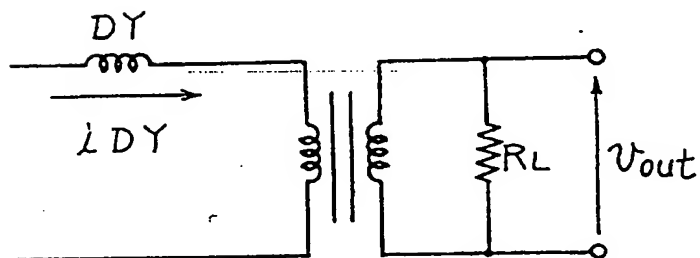


FIG. 10

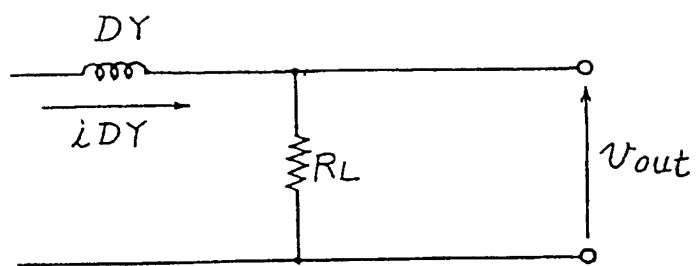


FIG. 11

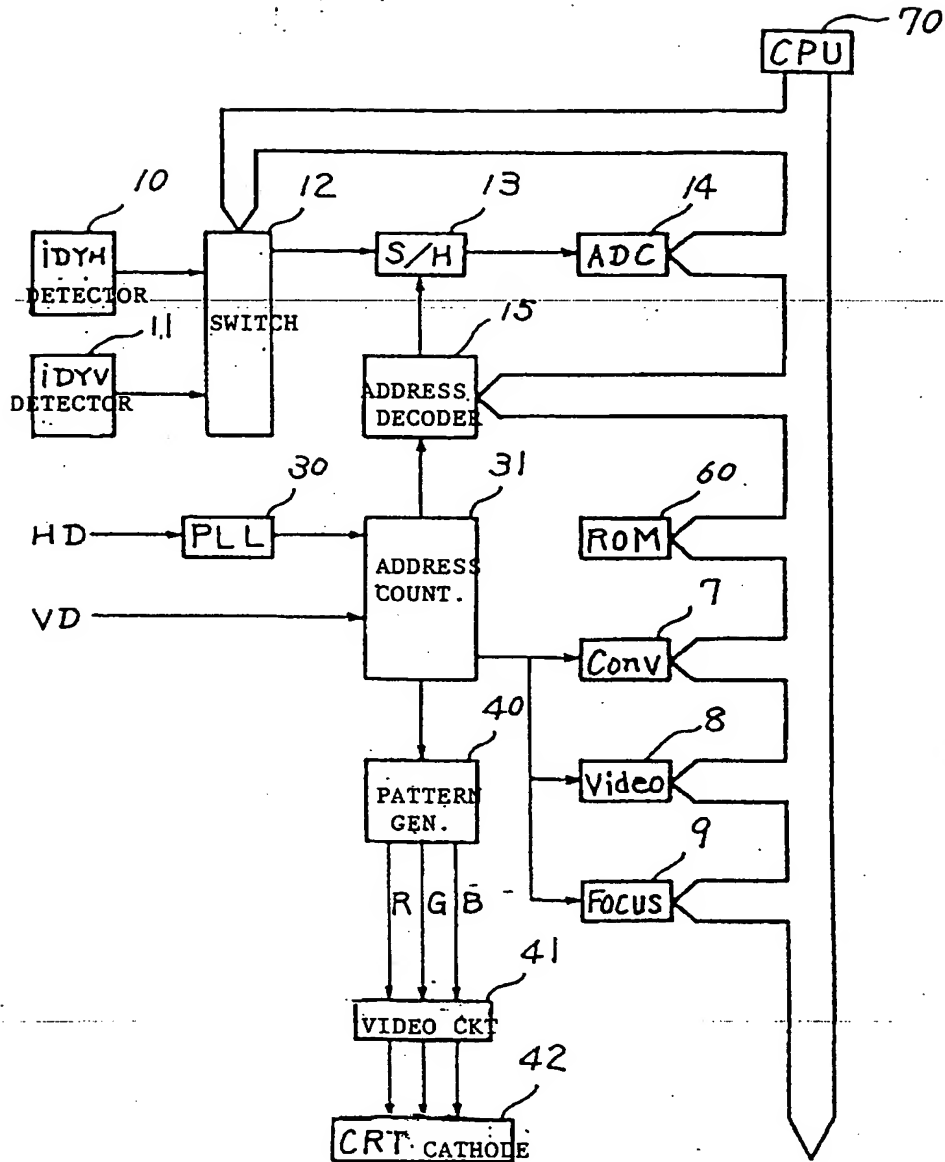


FIG. 12

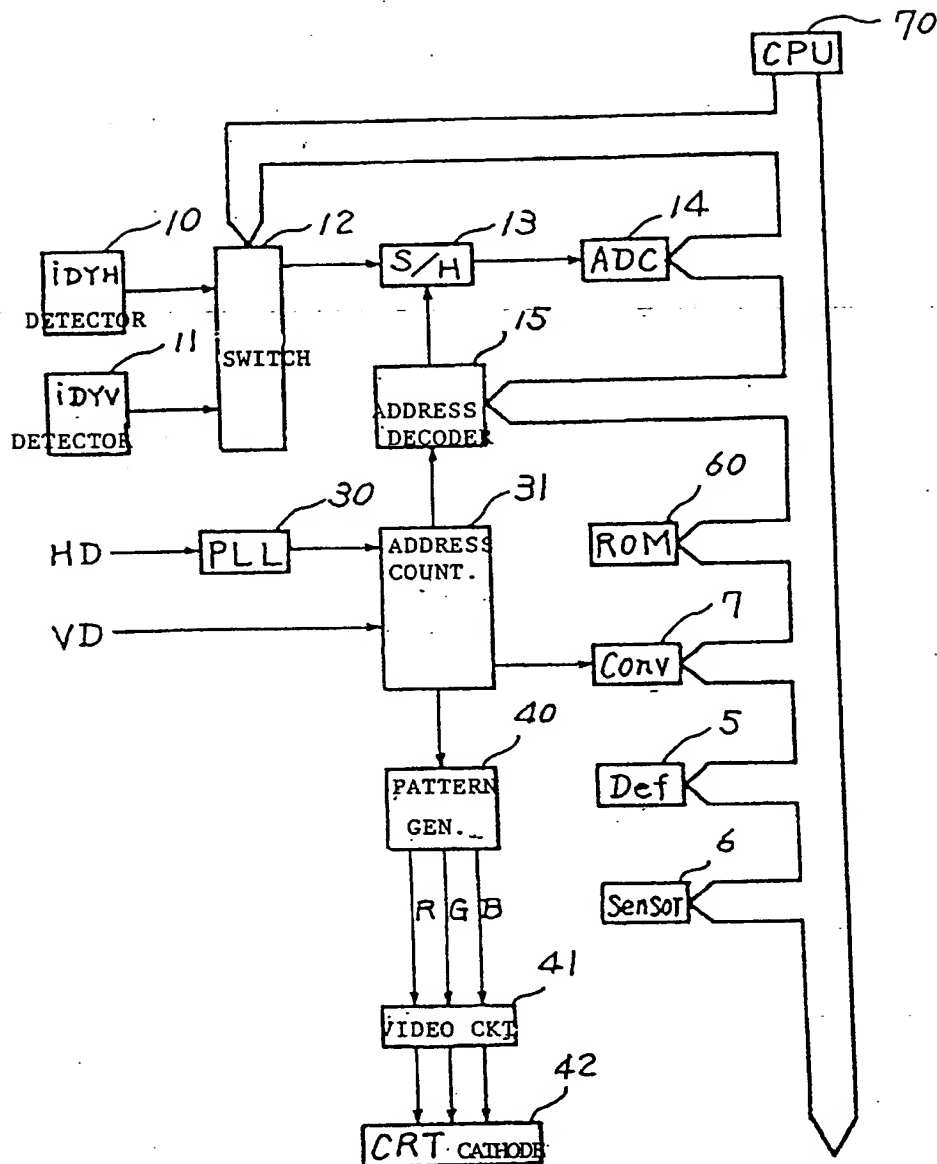


FIG. 13

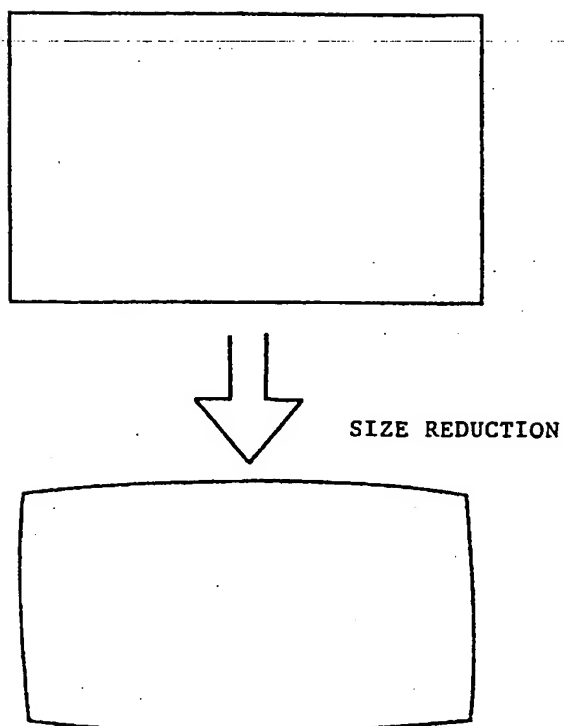


FIG. 14

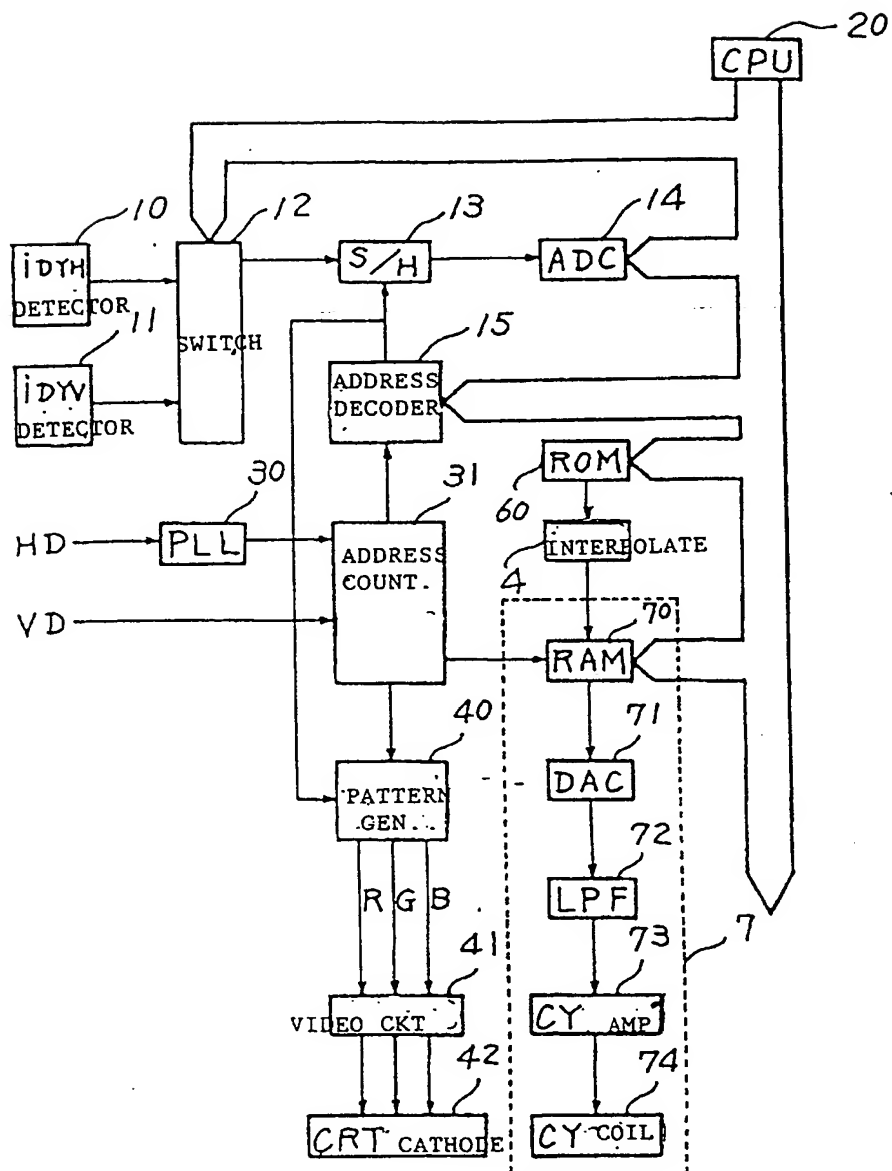
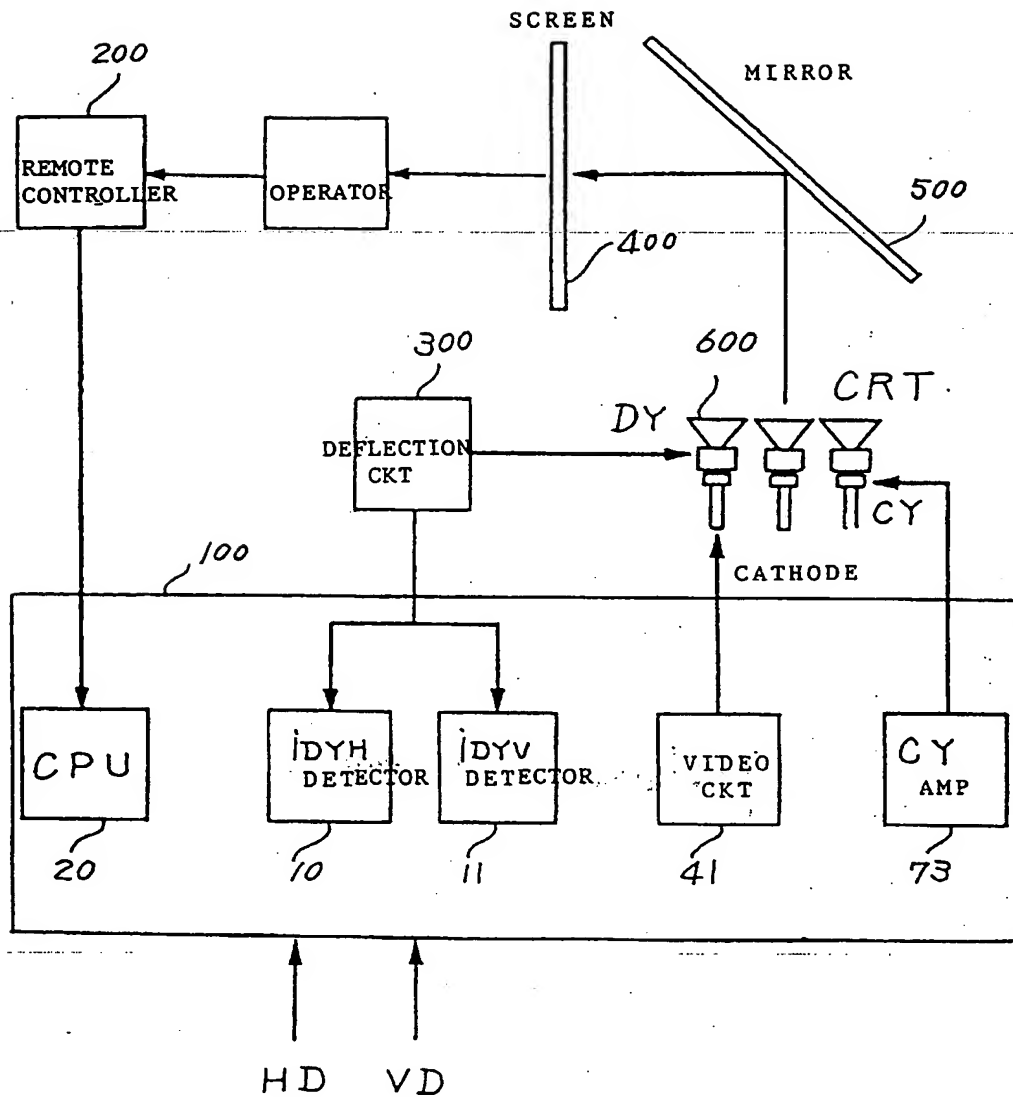


FIG. 15



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